

Design of an 80kV, 40A Resonant SMPS for Pulsed Power Applications

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Three Phase Resonant Power Supply



Designed to power a klystron tube

Power Supply Specifications

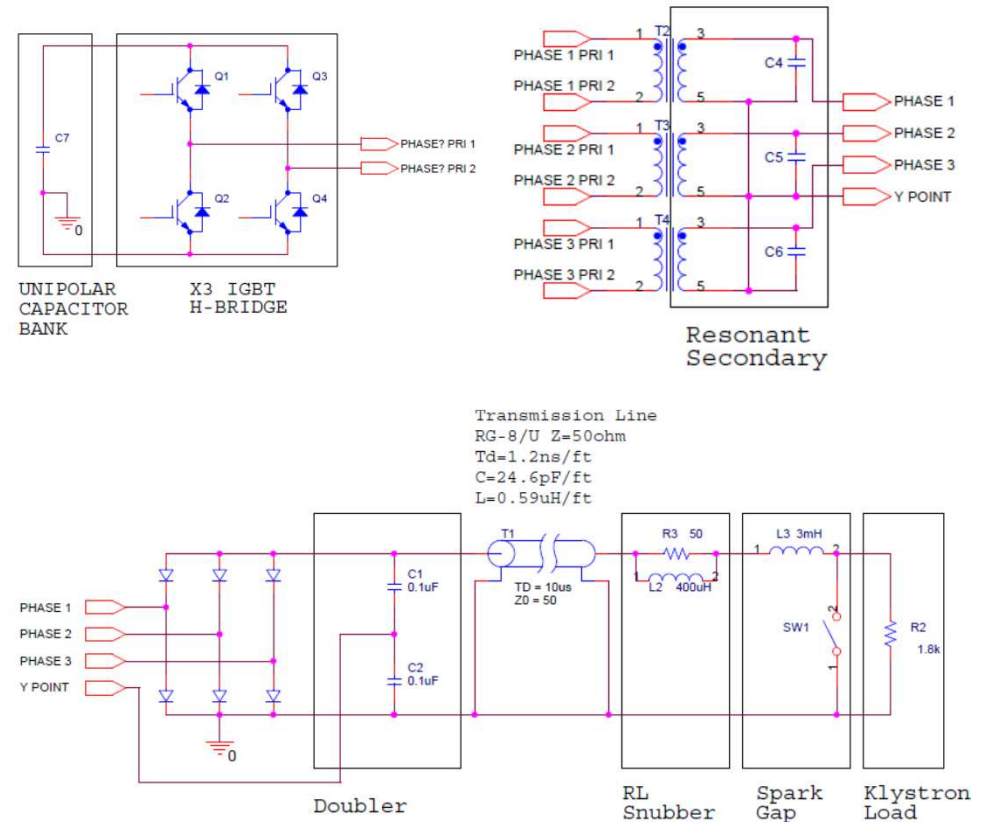
- Klystron tube requires -75kV to -80kV, 36A to 40A for 10ms
- Maximum output 95kV, 53A (5MW)
- Fast rise time (~ 0.3 ms)
- Low stored energy in filters
- Low voltage ripple
- Tolerant of load arcs
- Feedback control to compensate for capacitor bank voltage droop



Three Phase Resonant Power Supply



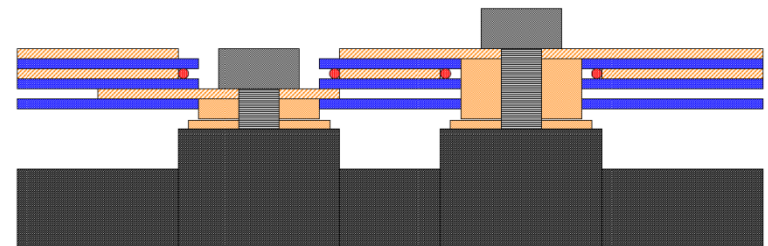
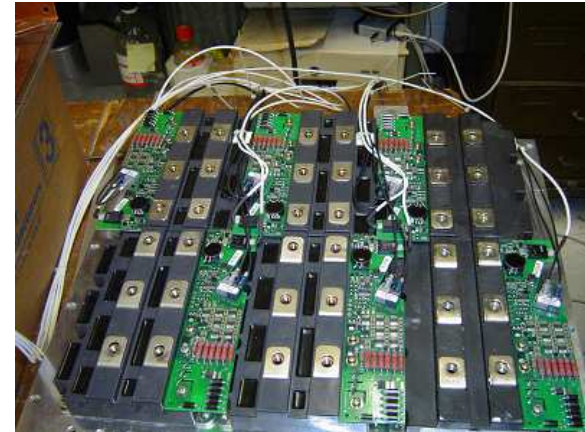
- Electrolytic capacitor bank:
 - 900V, 0.3F
- Full H-bridge per transformer
- Transformers have loosely coupled secondaries, parallel LC resonance
- 3 phase doubling configuration
 - Secondaries connected in Y
 - Y point connected to center of doubler capacitor
- RL snubber at the end of transmission line
- Crowbar sparkgap
- dsPIC microcontroller control system



IGBT H-bridges and Gate Drivers



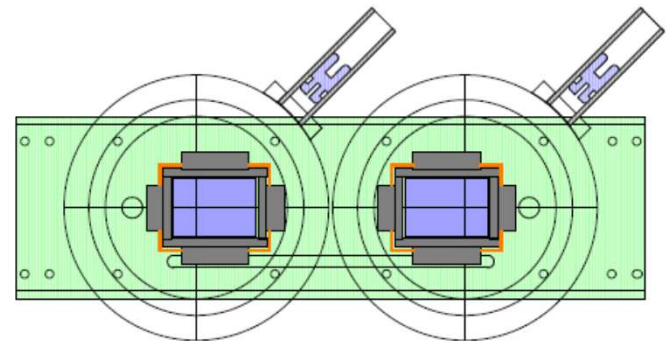
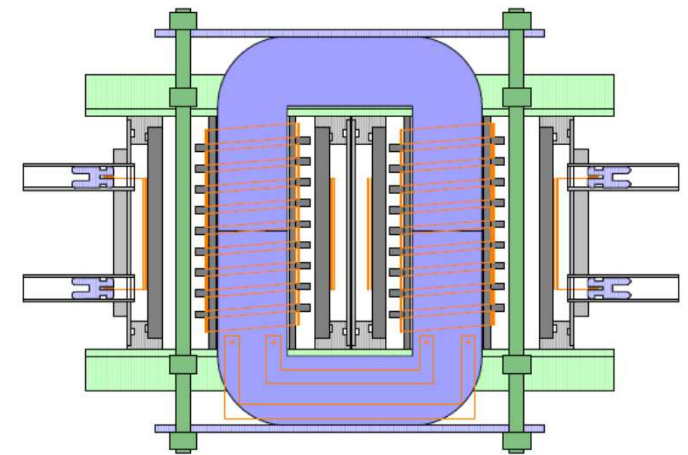
- Full H-bridge per transformer
- IGBTs: 3.3kV, 1.2kA (CM1200HB-66H)
- CT concepts plug and play gate drivers
 - Isolated from dc power supply
 - Fiber optic control
- Low inductance bus plates
 - 1/16" copper plates with 1/16" polycarbonate insulation
 - Low ESL stiffening capacitors



Resonant Transformer Design



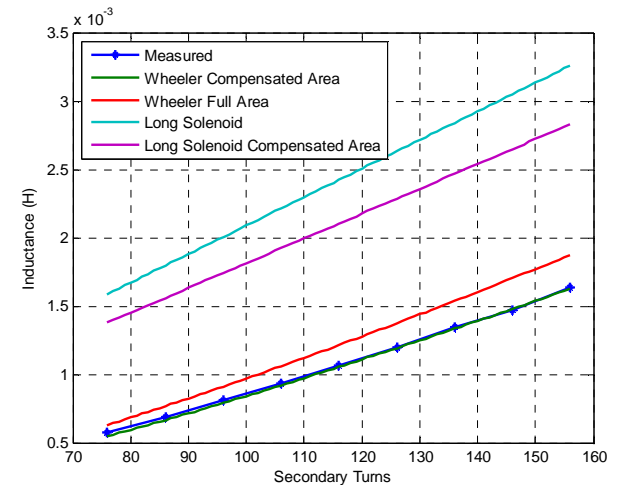
- Nano-crystalline iron core
- Loosely coupled secondary for high leakage inductance
- Parallel resonator capacitance 0.05uF
- Secondary leakage inductance 1.36mH
- 136 turn secondary
- 10 turn primary
- 120:1 boost ratio at resonance
- Oil immersed secondary for insulation and corona prevention



Resonant Transformer Model

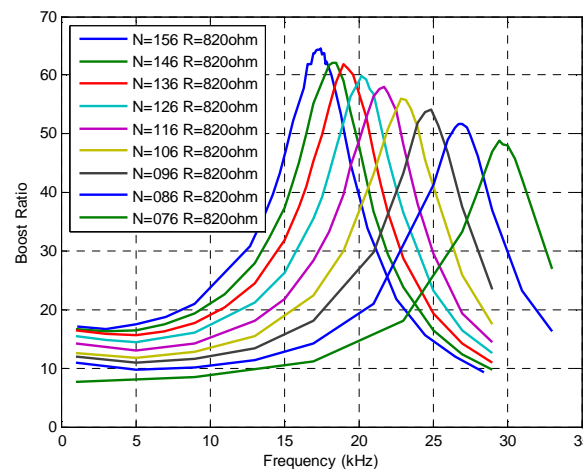
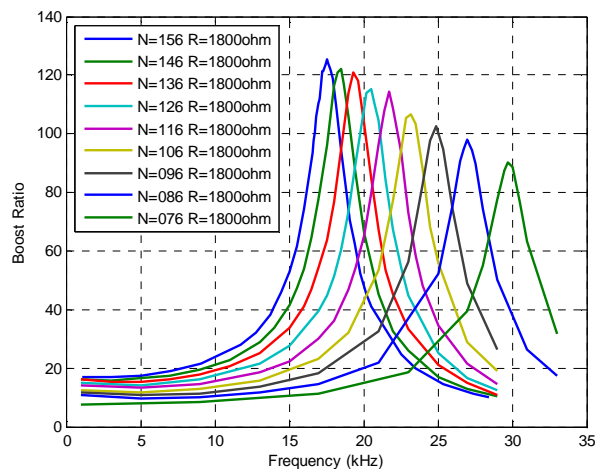


- Mathematical model of leakage inductance to avoid trial and error transformer design
 - Use Wheeler’s formula for a short solenoid
 - Assume magnetic flux is excluded from core when primary is shorted
 - Modify for leakage inductance by subtracting core area from coil cross section area



$$L_{long} = \frac{\mu_0 N^2 A}{h_{coil}}$$

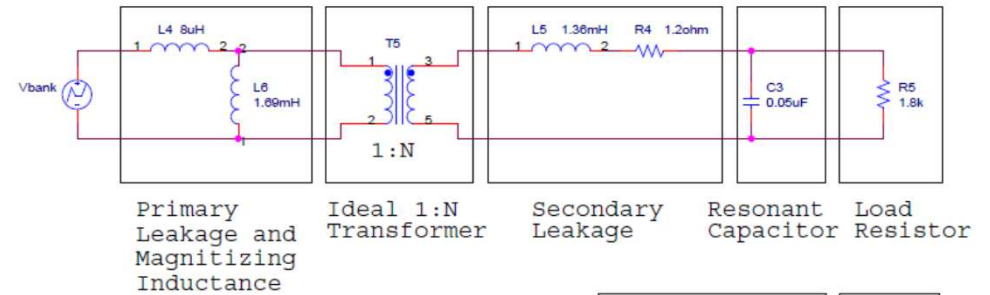
$$L_{wheeler} = \frac{10\mu_0 N^2 (A - A_{core})}{(9r_{coil} + 10h_{coil})}$$



Resonant Transformer Model

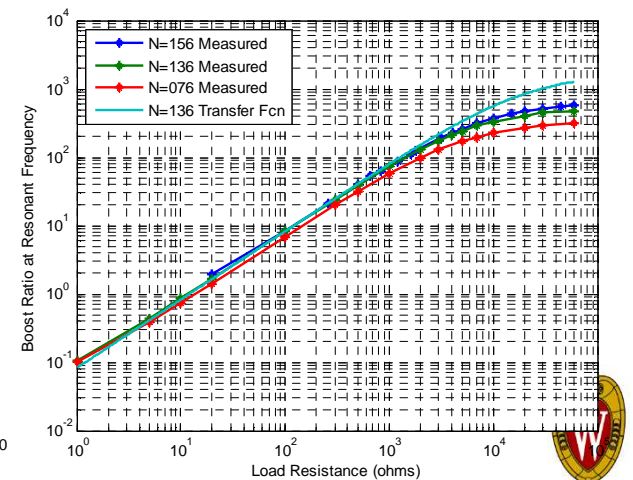
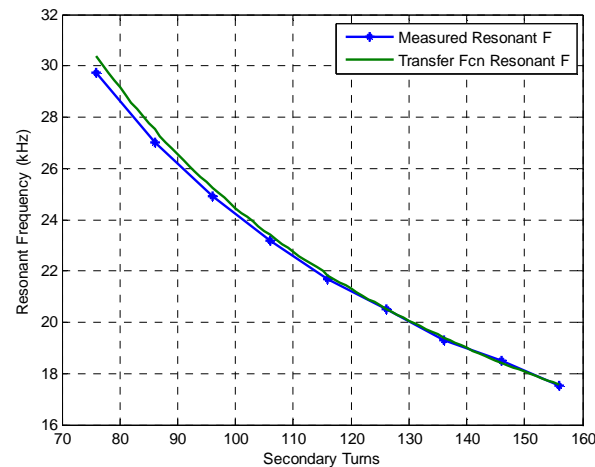
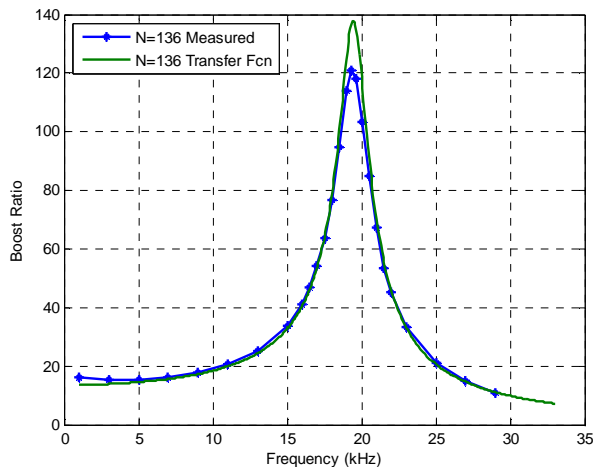
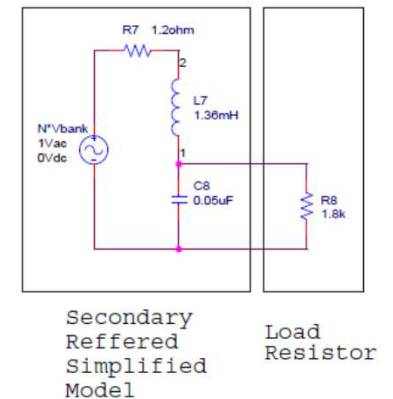


- Model of transformer boost ratio frequency response
- Transfer function from simplified secondary referred model
- Accurate prediction of resonant frequency and measured transfer function



$$\frac{V_{sec}}{V_{pri}} = \frac{N}{1 + (R_{inductor} + j\omega L) \left(\frac{1}{R_{load}} + j\omega C \right)}$$

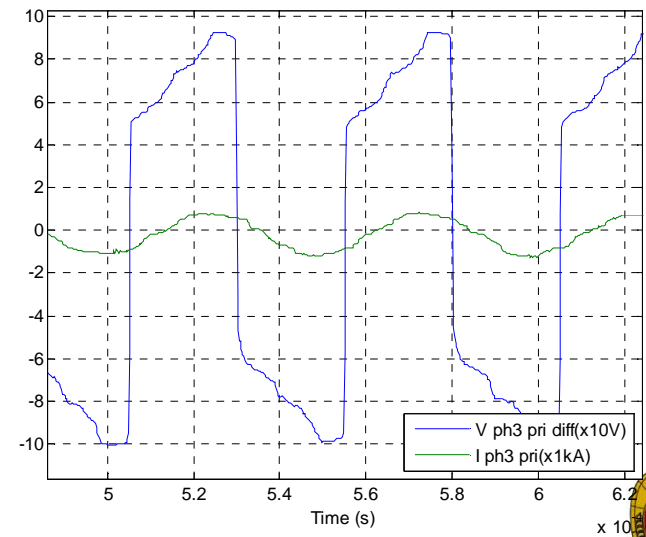
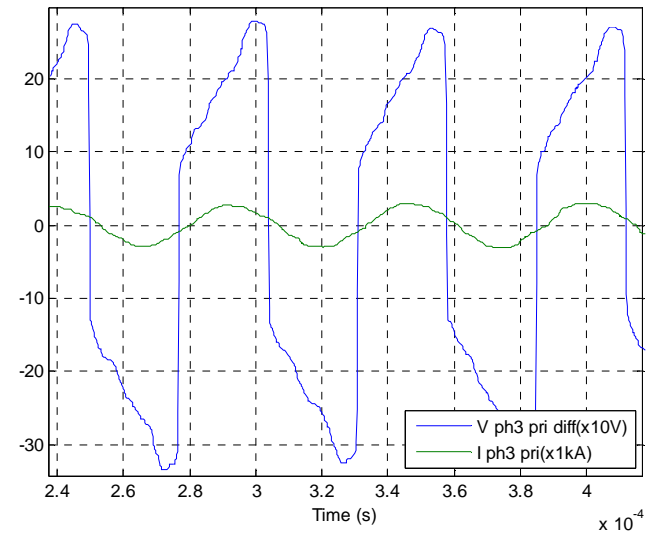
$$F_{res} = \frac{1}{2\pi} \sqrt{\frac{1}{LC} + \frac{1}{(RC)^2}}$$



Resonant Transformer Primary Waveforms



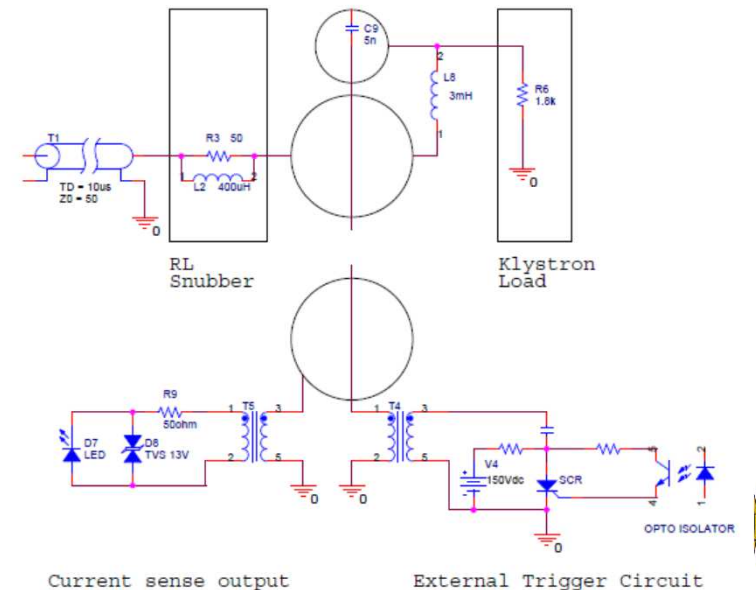
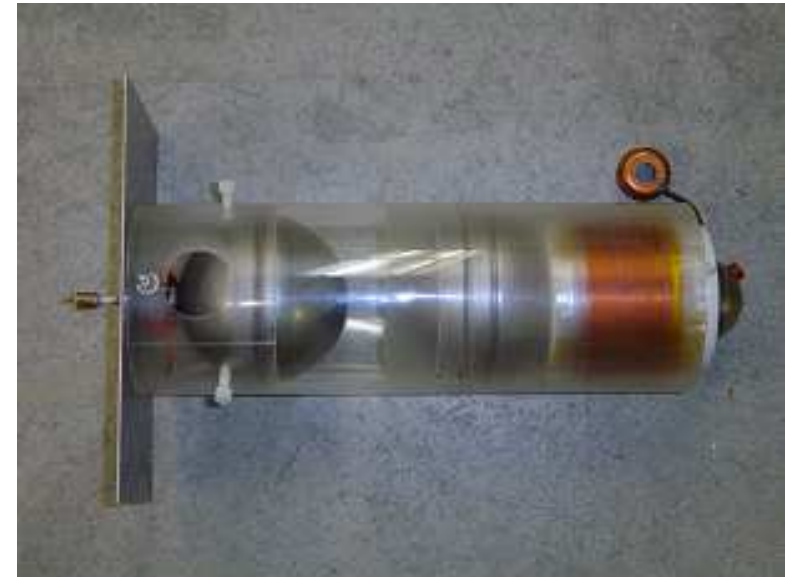
- Soft switching at resonance (ZCS)
- 18.5khz
 - Switching near zero current
- 20khz
 - Switching moves away from zero current



Crowbar Sparkgap



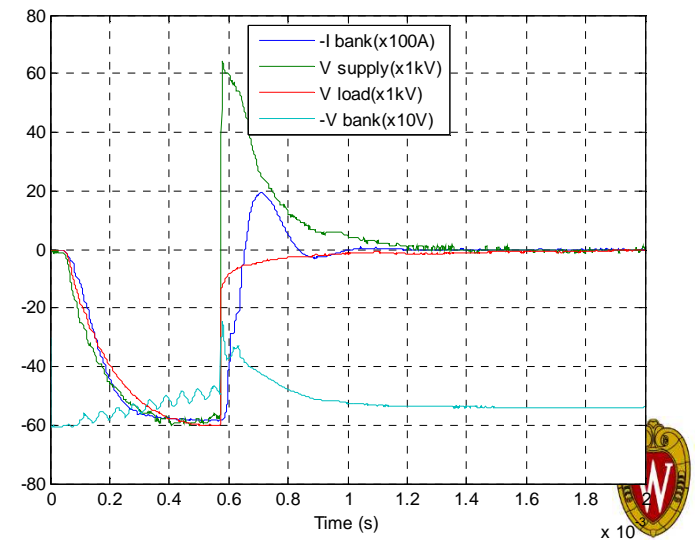
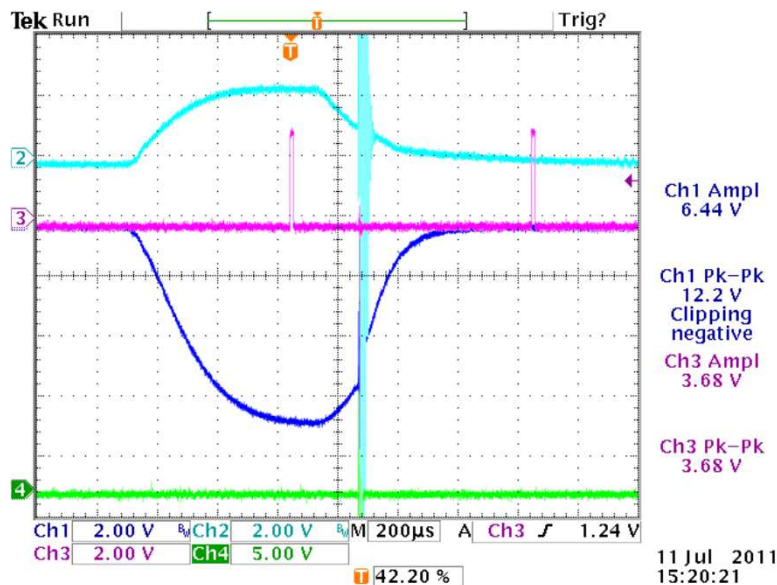
- In the event of an internal arc, damage to the klystron's cathode may occur
- 140J stored in doubler capacitors at 75kV
- Spark gap crowbars voltage across klystron tube in the event of arc.
- Methods of triggering
 - Overvoltage: Gap spacing
 - di/dt: series inductor connected to top trigger electrode
 - External trigger: connected to klystron RF detector
- Current sense output: shutdown signal to power supply if sparkgap fires.



RL Snubber



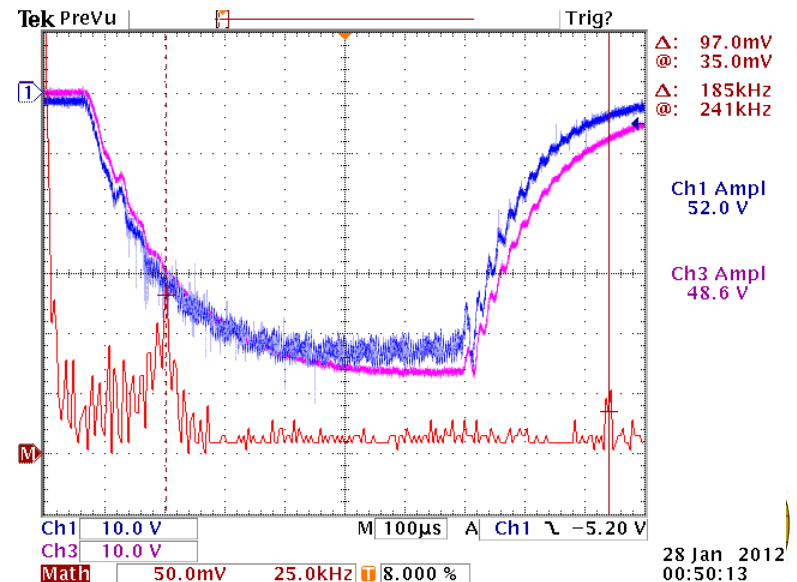
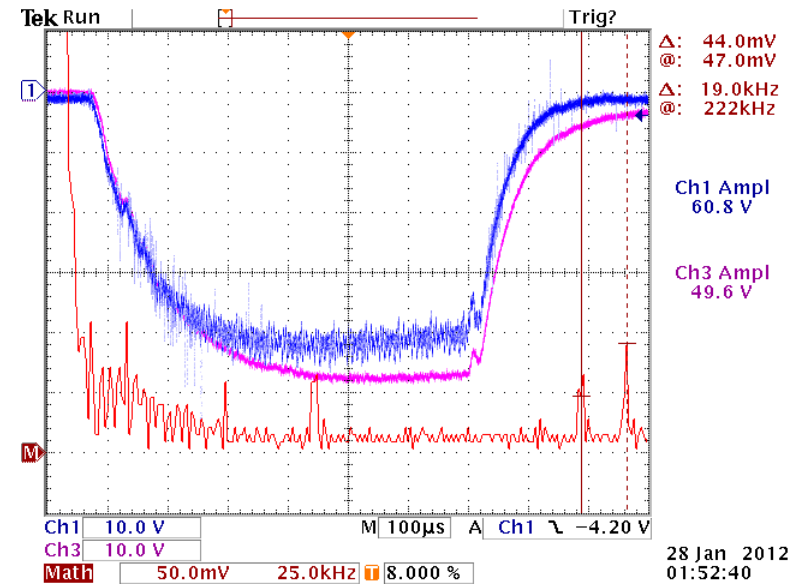
- Klystron arc generates HV pulse and ringing on transmission line
- Damage to doubling capacitors
- RL snubber added
 - $R=50\text{ohm}$, $L=400\mu\text{H}$
 - Series connection with Klystron
 - Mounted inside insulating PVC pipe
- Elimination of ringing, reduction of reflected pulse amplitude



Harmonic Mitigation and Filtering



- Three phase rectifier
 - 6th harmonic ripple
- Unbalanced secondary voltages
 - Variations in resonant frequency
 - Primarily 1st, 2nd, and 4th harmonics
 - Trimming of PWM duty cycle
 - Trimming resonant frequency by adding external inductance
- Lowpass Pi filter
- LC harmonic filter tuned to 6th harmonic

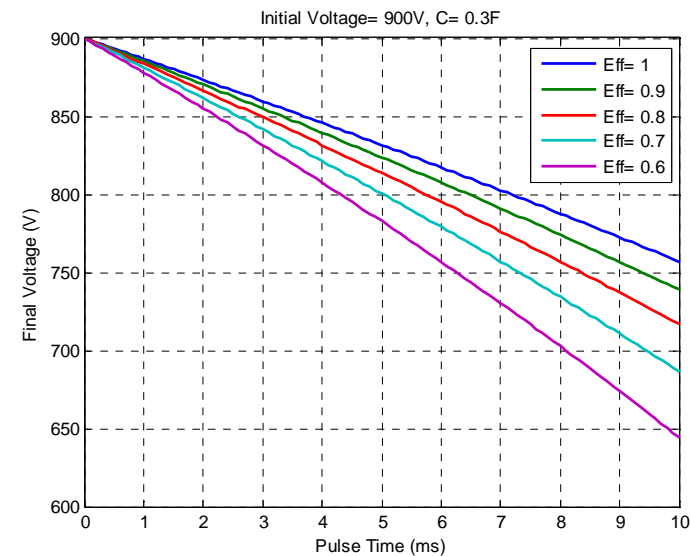


Control System



- Microchip dsPIC30F2020 microcontroller
 - Designed for SMPS use
 - 30 MIPS operation
 - High speed ADC (10bit, 2msps)
 - Time base synchronized PWM allows constant phase separation of primary waveforms
 - 120 control loop cycles per ms
- Fiber optic control of IGBT modules
- Ground loop isolated inputs

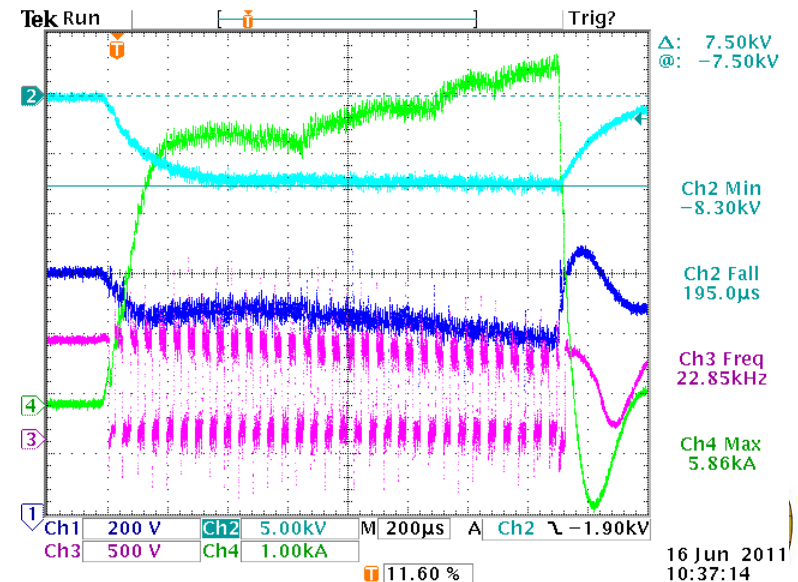
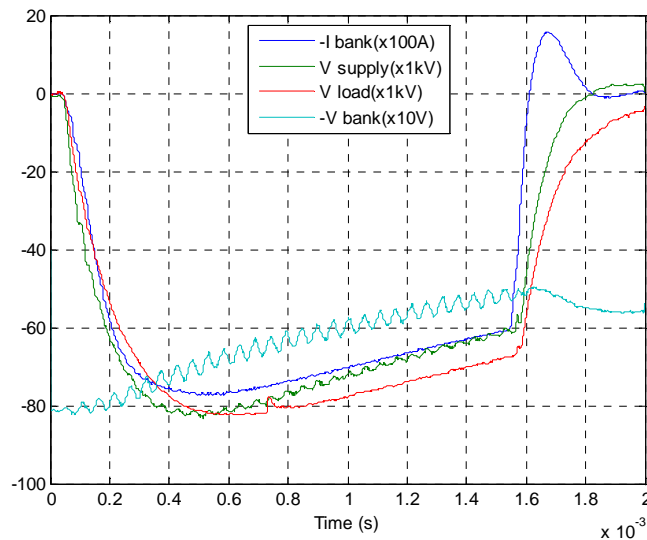
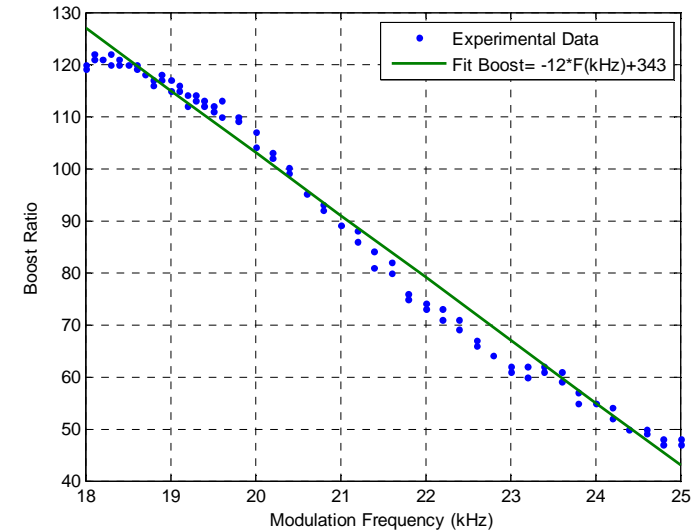
- Feedback/feedforward methods
 - Capacitor bank voltage: Operational
 - Output voltage: Development in progress



Control System



- Controller tunes switching frequency toward resonance to compensate for capacitor bank droop to stabilize output voltage
- Linearized approximation of boost ratio vs frequency
- $\text{Boost}(F\text{kHz}) = -12 \cdot F\text{kHz} + 343$



Questions?



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Scan me for email address.

